

Installation Guideline AZ®-800 & AZ®-750



After the successful market introduction of the AZ®-700 sheet pile range and 10 years of proven track record, ArcelorMittal has taken a further step in the development of wider Z-piles. As a result, the AZ®-800 range has been presented to the market in 2015. Intensive testing before market introduction showed that installation can be performed with standard pile driving equipment. However, the optimum choice of a sheet pile section requires a more rigorous analysis of the soil conditions. Nowadays, the existing ArcelorMittal sheet pile range allows designers and contractors to choose amongst a variety of profiles to best cater for the particular site conditions. Soil characteristics and driving methods are closely linked and have to be considered carefully.

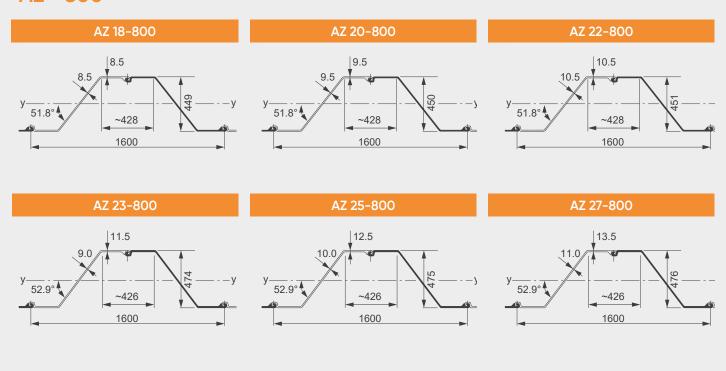
This document provides guidance to users towards selecting the profile for best execution results.

In case of further questions, please contact our Technical Department, your local ArcelorMittal office and check our online library:

sheetpiling.arcelormittal.com

Sheet pile sections Geometry

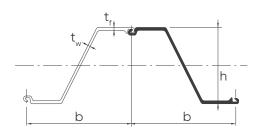
AZ®-800



AZ®-750



Sheet pile sections Special features



Section properties																		
Section	Width	Height	Thick	ness	Sectional area	Mo	ass	Moment of inertia	Elastic section modulus	Static moment	Plastic section modulus			Clo	SS ¹⁾			
	b	h	t _f	t _w		single pile	wall) GP	GP	G G P	ם ט	9 G	9 0 0 0	0 GP
	mm	mm	mm	mm	cm²/m	kg/m	kg/m²	cm ⁴ /m	cm³/m	cm³/m	cm³/m	S 240	\$ 270	\$ 320	0 000		S 46(\$ 500
AZ®-800																		
AZ 18-800	800	449	8.5	8.5	129	80.7	101	41320	1840	1065	2135	3	3	3 3	3	5 4	4	4
AZ 20-800	800	450	9.5	9.5	141	88.6	111	45050	2000	1165	2330	3	3	3 3	3	3	3	4
AZ 22-800	800	451	10.5	10.5	153	96.4	120	48790	2165	1260	2525	2	2	3 3	3	3	3	3
AZ 23-800	800	474	11.5	9.0	151	94.6	118	55260	2330	1340	2680	2	2	2 3	3	3	3	3
AZ 25-800	800	475	12.5	10.0	163	102.6	128	59410	2500	1445	2890	2	2	2 2	. 2	. 3	3	3
AZ 27-800	800	476	13.5	11.0	176	110.5	138	63570	2670	1550	3100	2	2	2 2	. 2	. 2	2	3
AZ®-750																		
AZ 28-750	750	509	12.0	10.0	171	100.8	134	71540	2810	1620	3245	2	2	2 2	: 3	3	3	3
AZ 30-750	750	510	13.0	11.0	185	108.8	145	76670	3005	1740	3485	2	2	2 2	2 2	2 2	3	3
AZ 32-750	750	511	14.0	12.0	198	116.7	156	81800	3200	1860	3720	2	2	2 2	2 2	2 2	2	2

¹⁾ Classification according to EN 1993-5. Class 1 is obtained by verification of the rotation capacity for a class-2 cross-section.

To optimise the design of a steel sheet pile wall according to EN 1993-5, use our free software *Durability* or contact our technical department. Tailor made profiles can be rolled on request.

- > 31 m rolling length possible, longer piles on request
- > Delivery possible in steel grades up to S 500 GP and exclusive AMLocor quality
- > High quality crimping of double piles for special applications
- > Excellent weldability because of low carbon equivalent value
- > Proven interlocking system with enhanced water tightness
- > Available as EcoSheetPile™ Plus, made from 100% recycled steel and with 100% renewable electricity, for the lowest possible carbon footprint

Choice of section

Once the static calculation is done and section modulus, pile length as well as steel grade are defined, it has to be checked, whether length of pile and section modulus are adequate for installation in the given soil conditions.

A well prepared geotechnical investigation should always be the basis for design and pile driving evaluation.

The following graph shall provide guidance for pile selection with respect to driving conditions.

Drivability of sheet piles in regard to length, soil conditions, section modulus and delivery form (pairs) for standard sheet pile walls is shown in the graph adapted from chapter eleven of the ArcelorMittal Piling Handbook, 9th edition, where further details and recommendations can be found.

As general rule of thumb it can be assumed that: "the recommended sheet pile length in [cm] corresponds to the section modulus in [cm³/m]". However, soil conditions have to be checked carefully.

Example: AZ 20-800

- > 2000 cm³/m section modulus;
- > Recommended length max. 16-20 m for soil condition "Easy".

Please note: this rule of thumb does not apply to combined walls, but is given only for standard sheet pile walls. For HZ®-M type or other combined walls, installation has to be checked rather in regards to existing soil conditions and required length of piles.

The wider piles will have less plugging effect at the pile toe in certain soil conditions, but more surface friction has to be expected. Changing from an AZ 26-700 to an AZ 25-800 will increase the surface area by roughly 9%. This should be considered when choosing the driving equipment.

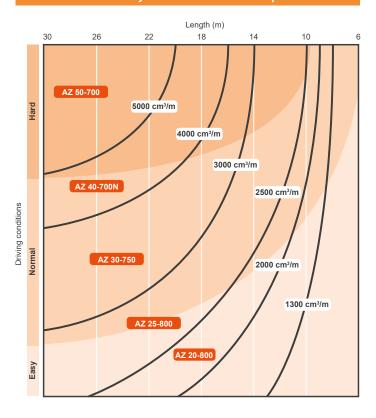
Installation aids, like water jetting or pre-drilling, can be foreseen, depending on prevailing soil conditions.

Water jetting is most effective in non-cohesive soils, while pre-drilling should be considered rather for cohesive soils. Both methods will facilitate installation, reduce necessary piling energy and minimize the effect of vibrations along adjacent buildings.

Soil definitions

	SPT val	ue (blows)	CPT value (in MN/m²)			
	Cohesive	Non-cohesive	Cohesive	Non-cohesive		
Easy	0 - 5	0 - 20	0 - 0.5	0 - 7.5		
Normal	5 - 15	20 - 40	0.5 - 1	7.5 - 15		
Hard	> 15	> 40	> 1	> 15		

Drivability of double AZ® sheet piles



Installation methods Vibrator and impact hammer

Installation of the AZ $^{\circ}$ -800 & AZ $^{\circ}$ -750 piles is possible with all standard installation methods:

- > vibratina
- > impact hammering
- > pressing

Installation with vibratory hammer

The dimensioning of piling equipment is generally driven by equipment availability and contractor's experience. Calculation formulae or curves and tables can be found in the ArcelorMittal Piling Handbook or in the recommendations of the machine manufacturers.

The connection between pile and vibratory hammer is the clamping device. The clamping force shall be more than 1.2-times the centrifugal force (in kN) of the vibratory hammer. The surface of the clamps shall be large enough and not worn-off to prevent damage to the pile head.

Installation is still often done with a single-clamp setup, gripping the pile over the middle interlock.

This method introduces forces out of the center of gravity of the wall and causes bending in the pile head, as well as additional friction in the adjacent interlocks. The use of single clamps is acceptable, but the preferred option should always be a double clamping system, to avoid damage to piles and driving equipment.

For piles with a width of 700 mm and larger, ArcelorMittal recommends the use of double clamps for double-Z piles, as the energy loss due to flapping ends can cause slower installation progress.

The benefit of using double clamps is especially given when installing AZ-800 double piles.

In addition, it is recommended to have the piles crimped or welded to avoid differential movements of the double pile under the clamps.

Turning plates for the different web angles are available from all major piling equipment manufacturers. In case of need, ArcelorMittal can provide contact details.

Dimensioning of driving forces can be done according to the existing methods, but close attention has to be paid to the soil conditions.

In soil conditions that are prone to plugging, horizontal stiffening plates or strips can be affixed slightly recessed from top or bottom end of pile. This is beneficial as the effects on pile driving caused by the soil plug is reduced. Hence, aiding in achieving installation tolerances (e.g. wall length, inclination, design depth).



Leader-mounted vibratory hammer with double clamps.

Installation with impact hammer

Today's standard machines are either hydraulic or diesel hammers; steam hammers are no longer in use. Fast-acting airdriven hammers are available and can be used for all pile sizes.

It is essential to use a correctly sized driving cap. The cap shall cover all of the pile area, leaving free the outside interlocks. The driving of double piles is to be preferred. The driving cap must be sufficiently rigid to transfer safely the impact energy from the hammer into the pile. Driving caps can be custom-made by the contractor, requested from the hammer manufacturer or can be obtained from ArcelorMittal on request for the use with diesel or free-fall hammers. Care shall be taken not to overstress the pile or the cap during driving.





Installation methods Driving caps

Sheet pile sections and corresponding driving caps

Arrangement	D ¹⁾	D ¹⁾
Driving caps	ZD 800 A	ZD 800 B
AZ®-800		
AZ 18-800	✓	
AZ 20-800	\checkmark	
AZ 22-800	\checkmark	
AZ 23-800	✓	✓
AZ 25-800	✓	✓
AZ 27-800	✓	✓
AZ®-750		
AZ 28-750		√
AZ 30-750		✓

¹⁾ D = Double pile.

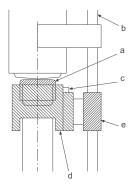
AZ 32-750

Sliding guides

Sliding guides are designed to guide the driving cap along the leader, thus guaranteeing proper alignment of the hammer in the centre of the driving cap. The adaptation to the leader is normally carried out on-site.

	Dimensions		Designation	Corresponding driving caps
500	70	410	500/90	ZD 800 A-weld ZD 800 B-weld
700	70	460	700/90	ZD 800 A ZD 800 B ²⁾

Arrangement of driving caps





b = leader

c = sliding guide

d = driving cap

e = leader slide

The leader slide (e) is not provided by ArcelorMittal.



Driving cap for impact hammer.

²⁾ Availability to be checked at time of order placement.

Installation methods Pressing

Installation by pressing

Especially in inner-city areas, pressing has become a standard vibration-free installation technology. Two types of presses are available on the market:

- > self-walking presses;
- > leader guided systems.

The width limitation of the self-walking systems today is at 1.40 m, length limitation of the section depends on the soil conditions, but is normally between 15–19 m. Pre-drilling and water-jetting are possible to improve the working progress.

Leader guided presses do exist for the AZ-800/AZ-750 profile series. The availability of equipment has to be checked with the specific manufacturers. It should be considered that more surface friction has to be overcome with the wider piles and that the pressing machine must have sufficient rigidity and power reserves to press the piles in the ground safely.

Pressing and vibrating can be facilitated by filling the interlock with lubricants, such as Beltan®Plus, grease or foam. A bolt at the end of the leading interlock in driving direction also prevents soil from entering the interlocks, as densified soil inside the interlocks may cause additional resistance while driving.



Self-walking press.



Leader guided pressing system.







Bolt inserted in leading interlock.

Soil conditions

A well prepared soil investigation is key to a successful project.

SPT/CPT tests, together with additional core drilling in the axis of the future structure, should be done to allow for the best possible evaluation of the intended working methods in regard to existing soil conditions.

In general, pile driving is possible in all kinds of soil, even in weathered rock, provided the piling method and pile section are chosen correctly.

Non-cohesive soils are best suited for vibrating. If SPT values > 50 blows prevail, additional water-jetting should be considered. If there is a high content of fine particles (< 0.1 mm), filling of the leading interlocks with foam, Beltan®Plus or grease is strongly recommended.

In situations with SPT values > 45 blows, a strong Z-pile with minimum elastic section modulus $W_{\rm el}$ of 2500 cm³/m should be selected. Length recommendation as mentioned on page 4 shall be verified.

General rule of thumb: "the harder the soil, the stronger and stiffer the sheet pile section should be".

Cohesive soils are best suited for impact pile driving; if vibration is used, a high amplitude is demanded. If CPT values > 1.0 MPa prevail, additional pre-drilling and strengthening of the pile toe with plates or rock shoes can be considered. Soft cohesive soils are suitable for pressing.

In situations with CPT values > 1.0 MPa, a strong Z-pile with minimum $W_{\rm el}$ of 2500 cm³/m should be used. Length recommendation as mentioned on page 4 should be verified. In general, installation of AZ® single piles is not recommended.

Installation in **soft or weathered rock** (< 5 MPa compression strength) is possible with high capacity impact hammers and sheet pile section modulus > 3600 cm³/m. Toe strengthening, pre-drilling or cutting with a trench cutter can be considered, depending on rock condition and driving depth.



Combined walls

Combined walls consist of high-inertia and massive primary elements, like HZ®-M beams, sheet pile box piles or tubes, with standard sheet piles as intermediary sheet piles in between.

The new AZ 20-800, AZ 25-800, AZ 30-750 and their derivates can be used as intermediary piles for combined walls.

The preferred choice of intermediary sheet pile is the AZ® double pile. Because of the location of the middle interlock, a natural rotation capacity is given.

The maximum theoretical swing α in every Larssen interlock is 5°, depending on the length of pile. The rotation is only geometrical, no additional tension is introduced into the section. A special crimping setup allows keeping the rotation capacity in the lower part of the sheet pile in case piles are ordered with crimping from the mill.

According to the standard delivery conditions based on EN 10248, the tolerance of a double pile is \pm 3% of the pile width:

	Width	Tolerance
AZ 18	1.26 m	+/- 3.8 cm
AZ 18-700	1.40 m	+/- 4.2 cm
AZ 18-800	1.60 m	+/- 4.8 cm

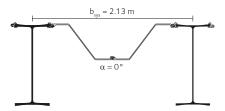
For a combined wall system this means that a difference of 7-10 cm can occur, with marginal material deformation.

In hard soil conditions, toe strengthening can be taken into account. In addition pre-drilling or water jetting might be necessary to install the intermediary piles safely.

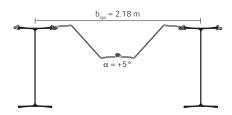
In general, the intermediary piles have 70-80 % of the length of the king piles; the exact length shall always be determined for each specific project.

For lifetime reasons, a minimum wall thickness of 10 mm in freshwater or seawater structures should be considered.

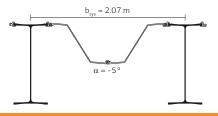
System width example: HZ 1080M A-12 / AZ 25-800



Theoretical system



Wider system



Narrower system

Technical assistance



Project references AZ®-800 & AZ®-750

Project location	Section	Application	Total tonnage	Productivity Piles/day	Page
Limelette, BE	AZ 25-800	Pile driving test	20	n.a.	12-13
Goole, GB	AZ 30-750	Flood protection	1300	20	14
Lauwersoog, NL	AZ 30-750	Quay wall	670	15	15
Penang, MY	AZ 30-750	Erosion protection	13750	12	16
Biblis, DE	AZ 20-800	Flood protection	1500	20-30	17
Saint-Laurent-du-Var, FR	AZ 25-800	Flood protection	2590	n.a.	18
Bocholt, BE	AZ 20-800	Erosion protection	2740	25	19
Vlissingen, NL	AZ 23-800	Quay wall	400	8	20
Brussels, BE	AZ 27-800	Parking	450	n.a.	21
Oslo, NO	AZ 23-800	Railway tunnel	2900	16	22
Zeeland, NL	AZ 25-800	Pile driving test	10	n.a.	23
Hamburg, DE	AZ 25-800	Foundation works	240	n.a.	24
Amsterdam, NL	AZ 18-800	Retaining wall	1200	8	25
Cape Town, ZA	AZ 25-800	Pile driving test	7	n.a.	26
Usedom, DE	AZ 25-800	Quay wall	375	6	27
Bremerhaven, DE	AZ 25-800	Quay wall	620	6	28
Copenhagen, DK	AZ 30-750	Pile driving test	6	n.a.	29
Rabat, MA	AZ 25-800	Parking	1320	4-8	30
Antwerp, BE	AZ 18-800	Bank protection	260	8-10	31
Stuttgart, DE	AZ 18-800	Retaining wall	448	20	32
Leiden, NL	AZ 18-800	Erosion protection	720	20-30	33
Karlsruhe, DE	AZ 18-800	Road tunnel	3944	14	34
Lokeren, BE	AZ 18-800	Underpass	373	20	35
Val de Reuil, FR	AZ 18-800	Foundation works	95	n.a.	36
Guaiba, BR	AZ 18-800	Retention basin	739	8-12	37
Haifa, IL	AZ 28-750	Service tunnel	6337	n.a.	38
Troyes, FR	AZ 18-800	Flood protection	204	n.a.	39
Dethlingen, DE	AZ 25-800	Cut-off wall	1138	8-12	40
Makhambet, KZ	AZ 18-800	Cut-off wall	1684	6-10	41
Fehmarn, DK	AZ 23/25/27-800	Aggregate bunker	1743	10-14	42
Cabinda, AN	AZ 18-800	Quay wall	1822	6-8	43

Pile driving test | Limelette Belgium | 2015

Section

 AZ 25-800, comparison with AZ 26-700 and AZ 26-700N, 22.0 m length, S 355 GP

Type of structure

> Pile driving test

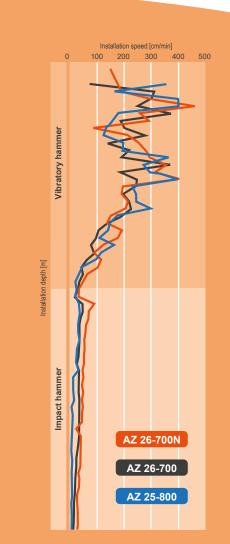
Equipment

- Vibratory hammer PVE 40VM installation depth 0 m to 8 m
- > Double clamp

Soil conditions

Silty clayey sand, middle dense in the upper part





Equipment

> Hydraulic hammer IHC S90 installation depth 8 m to 17 m

Soil conditions

Dense sand with hard layers in the lower strata

Job details

> Pile driving test with different sheet pile sections to prove drivability in hard soil conditions; admissible tension was not exceeded and installation speed was very uniform



Chantry Cottages | Goole Great Britain | 2015

Section

 AZ 30-750, 11.0 m length, S 355 GP, approx. 1300 t

Type of structure

> Flood protection

Equipment

- > PVE 38M vibratory hammer
- Standard frequency,
 1200 kN centrifugal force,
 38 kgm eccentric moment
- > Single clamp

Soil conditions

> Sand, clay, SPT 20-30 blows

- Quick execution,2-level driving guide
- Choice of section for durability reasons



Haven 22 | Lauwersoog The Netherlands | 2016

Section

 AZ 30-750, 20.0 m length, S 430 GP, approx. 670 t

Type of structure

> Quay wall with shiplift

Equipment

- > PVE 2319VM vibratory hammer
- High frequency,
 1100 kN centrifugal force,
 0-19 kgm eccentric moment
- > Single clamp DWK150T

Soil conditions

> Silty sand, SPT 30-40 blows

- > Maximum 10 minutes driving time per double pile
- Installation from land and water
- > 1-level guiding frame



Land reclamation | Penang Malaysia | 2016

Section

AZ 30-750 / AZ 20-800 / AZ 25-800,
 9.0 m up to 30.0 m length,
 S 430 GP, approx. 13750 t

Type of structure

> Erosion protection

Equipment

Vibratory hammer ICE 1412B
 with double clamp

Soil conditions

Dredged sand overlaying soft marine sediments

- Installation of 2 km cantilever Sheet Pile wall as erosion protection of an artificial island
- Pile driving from landside with 1-level guiding frame
- Installation of vertical drains to consolidate the soil
- Average installation performance up to 12 double piles per day



Weschnitzdeich | Biblis Germany | 2016

Section

 AZ 20-800, 9.0-12.0 m length, S 240 GP, approx. 1500 t

Type of structure

> Flood protection

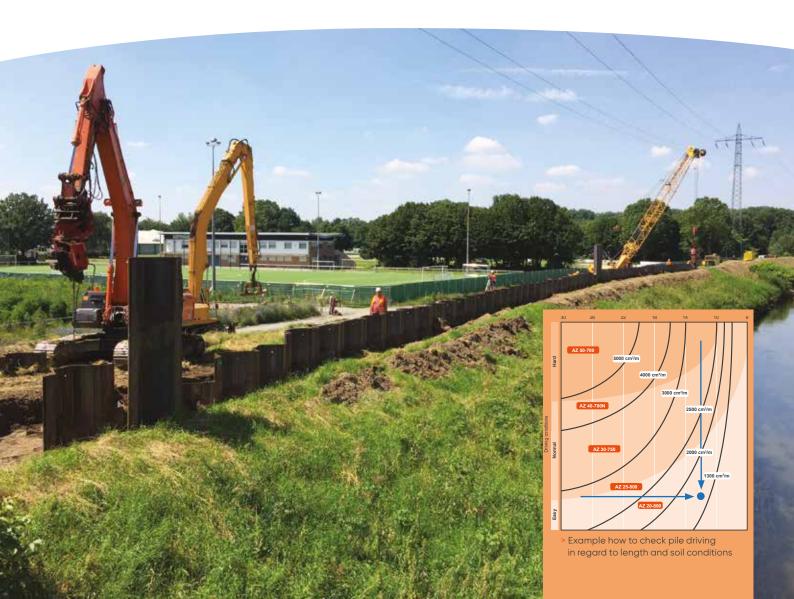
Equipment

- Müller MS 32HFV vibratory hammer
- High frequency, 1980 kN centrifugal force, 0-32 kgm eccentric moment
- > Double clamp

Soil conditions

> Backfill (loose), sand, SPT 10-20 blows

- High installation performance:20-30 double piles per day
- Interlocks filled with Beltan® Plus
- Use of Dixeran declutching detectors



Flood protection | Saint-Laurent-du-Var France | 2016

Section

 AZ 20-800^{-0.5} / AZ 23-800 / AZ 25-800, 15.0 m length, S 355 GP, approx. 2590 t

Type of structure

Flood protection

Equipment

- > PTC 23HFV vibratory hammer
- High frequency, 1360 kN centrifugal force, 0-23 kgm eccentric moment
- Single and double clamp
- Delmag D 19-52 diesel hammer with ArcelorMittal driving cap

Soil conditions

Backfill (compact), sand, SPT > 45 blows

- Driving test to prove performance of new AZ-800 piles
- Installation with vibratory hammer and diesel hammer
- > 2-level guiding frame
- Successful installation of AZ 20-800 in very hard ground conditions



Canal rehabilitation | Bocholt Belgium | 2016

Section

 AZ 20-800^{-0.5}, 6.0 m and 8.0 m length, S 355 GP, approx. 2740 t

Type of structure

> Erosion protection

Equipment

- > ICE 8RFSH vibratory hammer
- Normal frequency,
 436 kN centrifugal force,
 0-7.5 kgm eccentric moment
- Single clamp, excavator-mounted with swivel head

Soil conditions

> Sand (loose), clay (soft)

- Cantilever wall for erosion protection along a canal
- Installation with floating equipment
- > 1-level driving guide
- Performance: up to 25 double piles per day



Quarleshaven | Vlissingen The Netherlands | 2016

Section

 AZ 23-800, 23.0 m length, S 355 GP, approx. 400 t

Type of structure

> Quay wall

Equipment

- > PVE 2350VM vibratory hammer
- High frequency,
 2900 kN centrifugal force,
 0-50 kgm eccentric moment
- > Double clamp PPK175T

Soil conditions

 Dense sand with stones, stiff clay, CPT > 30 MPa

- Tube-combi-wall for new quay structure in very hard ground conditions
- Installation of tubes with PVE110 and IHC S200 hydraulic hammer
- > 1-level driving guide
- > Performance: up to 8 AZ-800 double piles per day
- > Waterjetting or pre-drilling not permitted



Parking "Spiegel / Mirroir" | Brussels Belgium | 2016

Section

 AZ 27-800, 6.5 m-16.0 m length, S 355 GP, approx. 450 t

Type of structure

Permanent retaining wall for 3 level underground car park

Equipment

Piles placed in a CSM wall (Cutter Soil Mix) with PTC 30HFV

Soil conditions

> Sandy silty clay

- Anchoring not possible due to surrounding buildings
- > Top-down construction method used, where the basement floors act as strutting system
- Installation in a soil-mix-wall to prevent vibrations damaging surrounding buildings and to achieve water tightness during excavation
- Interlocks will be seal-welded after excavation



Follobanen | Oslo Norway | 2016

Section

 AZ 23-800, up to 18.0 m length, S 430 GP, approx. 2900 t

Type of structure

> Railway tunnel

Equipment

- > ICE 28RF, regular frequency machine with 1624 kN centrifugal force
- > RTG19 with MRV105 vibrator
- Leader-guided pressing was used in sensitive areas

Soil conditions

 Soft clays in the upper layers, SPT 10-20 blows, granite bedrock in the lower strata

- Sheet piles as permanent and temporary retaining structures for railway tunnel construction
- Use of Beltan®Plus sealing system
- Rockbolting as pile toe support
- > Pile splicing up to 54.0 m length
- Productivity: up to 16 double piles per day



Pile driving test | Zeeland The Netherlands | 2016

Section

AZ 20-800 and AZ 25-800,
 16.0 m length, S 430 GP

Type of structure

> Pile driving test

Equipment

 Resonator RD260 with single and double camp

Soil conditions

> Clays and sand, medium dense soil

Job details

Successful pile driving test to verify the drivability of the AZ-800 sheet pile range with the new resonating pile driving method



Foundation works steel mill | Hamburg Germany | 2017

Section

AZ 25-800, up to 20.8 m length,
 S 240 GP, approx. 240 t

Type of structure

> Retaining wall

Equipment

> PTC 30HFV with 1641 kN centrifugal force and hydraulic drop hammer

Soil conditions

> Sand, medium dense soil

- AZ 25-800 used as intermediary sheet pile for a combined wall with HZ 880M A & B
- Foundation of new walking beam furnace, installation close to existing structures



Foundation | Amsterdam The Netherlands | 2017

Section

 AZ 18-800, AZ 25-800 up to 17.8 m length, S 240 GP, approx. 1200 t

Type of structure

 Canal embankment and retaining wall

Equipment

 Hydraulic 4 cylinder leader-guided pressing system

Soil conditions

Loose to medium dense sand, reclaimed

- > Tender demanded installation without vibration
- Pressing is done in two steps with two machines to guarantee correct wall alignment
- Average productivity:8 double piles per day



Pile driving test | Cape Town South Africa | 2017

Section

 AZ 25-800, 12.0 m length, S 430 GP

Type of structure

> Pile driving test

Equipment

- Vibratory hammer PTC 23HF3 with 1360 kN centrifugal force
- Single clamp

Soil conditions

 Fine sand, ferruginised sand, SPT 45 blows

Job details

Pile test to prove drivability of the new sections in subtropical soil conditions



Quay wall | Usedom Germany | 2017

Section

- AZ 25-800, up to 28.25 m length,
 S 390 GP, approx. 375 t
- > HP400x122, length 22.0 m used as anchor piles, approx. 185 t

Type of structure

> Quay wall

Equipment

- Vibratory hammer Müller MS 23HFV with turning plate and double clamp
- Hydraulic hammer IHC S35

Soil conditions

 Organic soil, dense sand, stiff clay

- Sheet pile wall with one anchor level, installation on water, all equipment on barge
- Splicing of HP piles on job site to final length of 50.5 m
- > Presence of obstacles in the working area
- Average installation performance 6 double piles per day



Westkaje | Bremerhaven Germany | 2017

Section

- AZ 22-800, up to 22.45 m length,
 S 355 GP, approx. 620 t
- King piles 1620 x 16, up to 27.2 m length,
 S 355 J2H, approx. 2934 t
- HTM 600 x 136 as anchor pile, length up to 55.0 m, inclination 1:1, S 355 J2+M, approx. 1095 t

Type of structure

Quay wall

Equipment

- Vibratory hammers MS 32HFV and MS 48HFV, leader-guided with double-clamp setup
- > IHC S70 and S90 hydraulic hammers

Soil conditions

- Existing backfill, middle dense to dense sand, followed by hard silt layers
- Obstacles by old structures in the ground were encountered all over the construction area and had to be removed

- Demolition and rebuilding of 500 m existing quay wall, including deepening of the existing quay by 2.0 m
- Removal of numerous old foundation structures in the ground
- Delivery of anchor piles in partial length, splicing on site to final length, used as friction piles without jet-grouting
- > Total construction time 18 months; installation done on land and on water
- Average installation performance for intermediary piles: 6 AZ double piles per day piles: 6 AZ double piles per day



Pile driving test | Copenhagen Denmark | 2018

Section

AZ 30-750, 13.5 m length,
 S 355 GP, approx. 6 t

Type of structure

> Pile driving test

Equipment

> Junttan SHK 100-6 hydraulic hammer, leader-guided on PMx22 base carrier with adapted driving cap and drilling attachment

Soil conditions

The upper layer consists of silty sand, lower layer is mainly soft to medium stiff silty clay

Job details

 Pile test using multiple measuring devices to check vibration around the piling machine

- Piling very close to existing pipeline, distance < 1.0 m, with and without predrilling
- Predrilling with auger diameter 300 mm in the middle of a double pile
- Vibration impact significantly lower when predrilling is used



Underground car park | Rabat Morocco | 2018

Section

 AZ 25-800, 22.5 m length, S 430 GP, approx. 1320 t

Type of structure

> Temporary retaining wall

Equipment

- PVE 40VM vibratory hammer with turning plate and double clamps
- > Predrilling with 350 mm diameter
- > Two-level driving guide

Soil conditions

- > The soil consists of sand, followed by medium stiff clay and fine medium dense to dense sand
- Obstacles have been found between 8-12 m depth

- For the construction of a new underground car park, a temporary sheet pile wall is installed
- Filling of interlocks to facilitate later pulling-out of the sheet piles
- Deep-laying obstacles are removed with the help of the drilling machine
- Average daily production rate:4-8 piles



Bank protection | Antwerp Belgium | 2018

Section

AZ 18-800, 18.5 m length,
 S 355 GP, approx. 260 t

Type of structure

> Bank protection at oil terminal

Equipment

- PVE 50VM vibratory hammer with single clamp
- > IHC S90 impact hammer with special driving cap for AZ-800 sections

Soil conditions

> Silty clayey sand, partially dense

- Construction of a new retaining wall at the oil terminal
- Coating applied on the first3 meters of the sheet pile wall
- Filling of interlocks to reduce friction during pile driving
- Average production rate:8-10 piles per day



Retaining wall | Stuttgart Germany | 2018

Section

- AZ 18-800, 10.0 m length,
 S 240 GP, approx. 448 t
- AZ 32-750, 14.2 m length,
 S 240 GP, approx. 1010 t

Type of structure

> Retaining wall

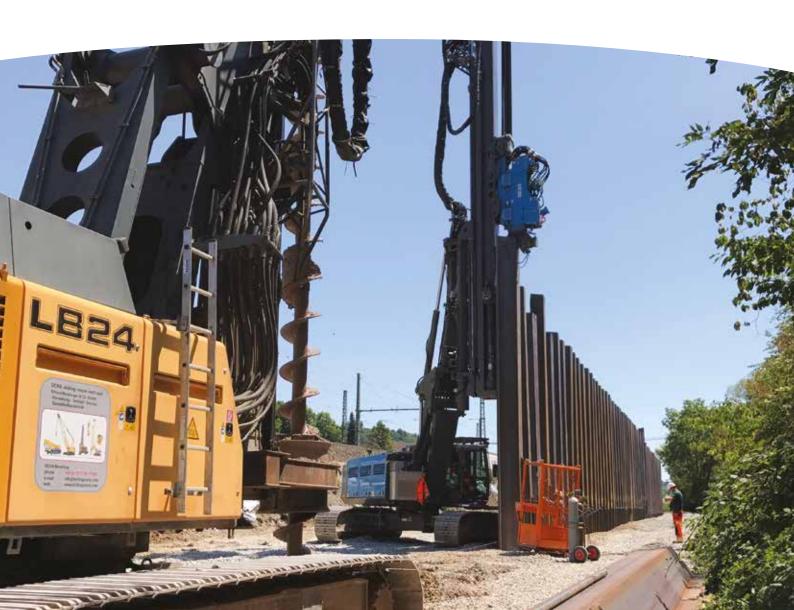
Equipment

- ABI TM22 with vibratory hammer MRZV 30VV with single clamp
- > Drilling rig LB24 with CFA attachment

Soil conditions

 Sand and gravel in the upper layers, penetration of pile toe into limestone formation

- Retaining wall with flood protection function for a railway crossing, in the frame of the "Stuttgart 21" project
- Predrilling to allow pile toe penetration into limestone
- Daily production up to 20 double piles



Erosion protection | Leiden The Netherlands | 2018

Section

- AZ 18-800, up to 13.0 m length,
 S 355 GP, approx. 720 t
- AZ 20-800, up to 11.0 m length,
 S 355 GP, approx. 320 t

Type of structure

> Canal embankment

Equipment

> ICE 14RF vibratory hammer with single clamp

Soil conditions

> Loose silty sand with peat lenses

- Replacement of an existing concrete wall by a long lasting anchored steel sheet pile wall
- Daily production 20-30 double piles



Road tunnel | Karlsruhe Germany | 2018

Section

- > AZ 18/20/23/25-800
- > AZ 28-750
- Up to 21.5 m length,
 S 240 GP, approx. 3944 t

Type of structure

> Inner city road tunnel

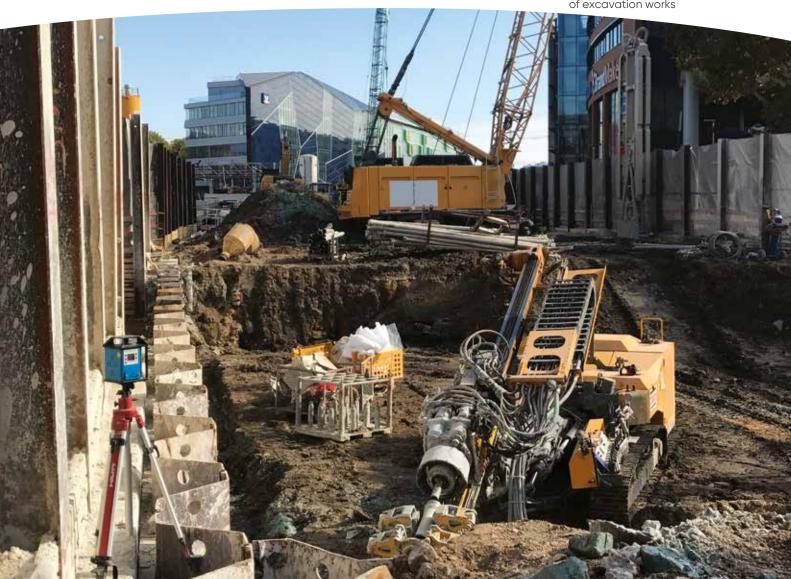
Equipment

- > Sheet pile placed in slurry wall
- Vibratory hammer Müller MS 32HFV as auxiliary piling machine

Soil conditions

> Gravel, silty sand

- Construction of a tunnel for a new metro line in the city center using sheet piles placed in a slurry wall
- Permanent sheet pile wall, acting as load bearing element, concrete connection by welded shear force transmitting elements
- > High demand for watertightness
- Limited space for construction and storage
- Daily production up to 14 double piles, depending on productivity of excavation works



Underpass | Lokeren Belgium | 2018

Section

AZ 18-800 and AZ 25-800,
 3.2 m up to 12.4 m length,
 S 355 GP, approx. 373 t

Type of structure

Underpass of railway line with access ramps

Equipment

 Various excavator mounted vibratory hammers (PVE, Movax)

Soil conditions

> Loose silty sand

- Vertical sheet pile installation in the tunnel area, inclined sheet pile installation 1:5 in the area of the ramps for aesthetical reasons
- Prefabricated connection elements for the special piles parts of the wall

- Pipes for inclinometer measurements preassembled
- > Temporary tubular struts until concrete base slab installed
- > Welding of interlocks after installation to achieve watertightness
- Productivity up to 20 double piles per day



Permanent outside wall for building | Val de Reuil France | 2018

Section

AZ 18-800, 6.50 m length,
 S 355 GP, approx. 95 t

Type of structure

Permanent load bearing wall for an industrial building

Equipment

 ABI TM13/16 equipped with MRZV600 and single clamp

Soil conditions

- Middle dense to dense Sand and gravel
- > SPT > 40

- The sheet pile sections are used as vertical bearing element for the final structure.
- > The piling layout is adapted to the geometry of the building, the necessary corner piles are manufactured on site, using C9 corner sections.
- A concrete capping beam will be constructed to connect the sheet pile wall to the superstructure.



Retention basin | Guaiba Brazil | 2019

Section

AZ 25-800, 18 m length,
 S 430 GP, approx. 739 t

Type of structure

Retention basin for a cellulosis factory

Equipment

> Müller MS 62

Soil conditions

- Predominantly medium stiff to stiff clay with sand up to approximately 10 m depth, followed by medium dense to dense sand with clay;
- > SPT 30-45

- Circular sheet pile structure with 100 m diameter
- > For the construction of the circle, no bent piles were needed, just interlock rotation was used



Tunnel | Haifa Israel | 2019

Section

 AZ 28-750 and 32-750, 16.0 m up to 20.50 m length, S 355 GP and S 430 GP, approx. 6.337 t

Type of structure

> Service tunnel

Equipment

- Müller MS62HFV, APE 200-6 with additional weight, PTC 48HFV
- Delmag D46-32

Soil conditions

- > Sand and clay
- > SPT 30-40

- Water tight retaining wall for the construction of a service tunnel, with temporary connection to concret base slab
- > Sheet piles will be used multiple times on the site
- Obstacles formed by large stones are to be expected



Flood protection | Troyes France | 2020

Section

- AZ 18-800, 8.0 m up to
 10.85 m length, approx. 204 t
- AZ 28-750, 11.45 m length, approx. 333 t, Steel grade S 355 GP

Type of structure

> Flood protection

Equipment

- > ABI MRZV925 leader guided
- PTC 17HFV und 23HFV free hanging on crawler crane
- Movax SH75 mounted on a 35 t
 -excavator

Soil conditions

Medium-dense to dense sands, medium stiff to stiff clay

- Sheet pile driving close to sensitive structures in innercity area
- Extensive measurement campaigns to check noise and vibration levels during execution of work
- AZ-800 piles used partially as intermediary piles for a combined wall with HZ880M B-14
- Sheet piles finally covered with steel or concrete capping beams



Cut-off wall | Dethlingen Germany | 2022

Section

AZ 25-800, 22 m length,
 S 240 GP, approx. 1138 t

Type of structure

> Cut-off wall with static function

Equipment

- > ABI TM22 with MRZV30VV
- High frequency, variable moment, 1500 kN centrifugal force, 0-30 kgm static moment
- > Single clamp

Soil conditions

Fine sand, peat, clay in varying locations

- > Securing of a military waste site
- > Pre-drilling to loosen clay layer
- Introduction of vertical loads from roofing structure using concrete capping beam



Cut-off wall | Makhambet Kazakhstan | 2022

Section

AZ 18-800, 8 m length,
 S 355 GP, total 1684 t

Type of structure

 Shore protection without static function

Equipment

- > Excavator-mounted vibro ESF7M
- > 604 kN centrifugal force
- > 7 kgm static moment
- > Single clamp

Soil conditions

> Silty sand, clay

- > Erosion protection
- Installation of 2609 single piles in jagged-wall setup



Retaining wall | Fehmarn Denmark | 2022

Section

> AZ 23/25/27-800, 18.7 up to 22.2 m length, S 355 GP, approx. 1743 t

Type of structure

> Aggregate bunker

Equipment

- > Liebherr LRB155 and LRH100
- Vibratory hammers ICE 28RFS, ICE 823B, ICE 6420
- > Impact hammer IHC S70
- > Single and double clamps

Soil conditions

> Sand, stiff clay

- Storage structure for aggregates
- Longitudinal walls in AZ 23-800, transversal walls in AZ 25-800 and AZ 27-800 around gates and openings



Quay wall | Cabinda Angola | 2022

Section

AZ 18-800, 8 m up to 20.5 m length,
 S 355 GP, total 1822 t

Type of structure

> Quay wall and wave breaker

Equipment

- > Vibratory hammer ICE 55NF, ICE 815
- > Impact hammer IHC S90 and PVE 9NL
- Single clamp

Soil conditions

Sand, stiff clay, conglomerat up to 30 Mpa strength

- Intermediary piles for a combined HZ 880M-A12 wall
- Installation in very hard soil (rock-like condition)



Documentation



Please refer to our website to download all our documentation: sheetpiling.arcelormittal.com or contact us via E-mail: sheetpiling@arcelormittal.com



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